

# Corrosion assessment of Zn-rich epoxy primers with carbon nanotube additions in an electrolyte with a bacteria consortium

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### *Abstract*

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Multifunctional coatings for corrosive environments have been developed to include two basic principle protection mechanisms: a barrier mechanism acting as a mass transfer process blocker, and cathodic protection mechanism acting as a charge transfer process promoter. Both mechanisms were assessed for Zinc-Rich Epoxy (ZRE) coatings in the presence of Carbon Nanotubes (CNTs) and exposure to a bioelectrolyte in order to study the evolution process during microbial corrosion conditions. The purpose of this study is to characterize in a comprehensive experimental platform the electrochemical response of a dual-protection zinc epoxy coating with different ratios of additive carbon nanotubes to active zinc particles upon exposure to a sulfate reducing consortium. Carbon nanotubes addition was found to affect both the prevailing mechanism at the coating interfaces and the formation of a biofilm at the coating surface that influenced the relatively dominance of the barrier protection mechanism. These multifunctional coatings with active particles could help to balance the charge transfer efficiency in terms of the sacrificial of zinc and barrier mechanisms, which influence biofilm formation and have potential consequences for biocorrosion on carbon steel.

### *Contribution to the field*

This work aims to determine the electrochemical behavior of a Zn-rich primer with MWCNTs additions in an electrolyte containing an SRB consortium. A few studies have evaluated Zn-rich epoxy primers in media containing sulfate reducing bacteria but to the best of our knowledge no studies have investigated Zn-rich primers with MWCNTs added to their matrix in an environment including a sulfate reducing consortium.

### *Ethics statements*

#### *Studies involving animal subjects*

Generated Statement: No animal studies are presented in this manuscript.

#### *Studies involving human subjects*

Generated Statement: No human studies are presented in this manuscript.

#### *Inclusion of identifiable human data*

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### *Data availability statement*

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# Corrosion assessment of Zn-rich epoxy primers with carbon nanotube additions in an electrolyte with a bacteria consortium

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Keywords: zinc-rich epoxy coatings, carbon nanotubes, biocorrosion, sulfate-reducing microorganisms.

## Abstract

Multifunctional coatings for corrosive environments have been developed to include two basic principle protection mechanisms: a barrier mechanism acting as a mass transfer process blocker, and cathodic protection mechanism acting as a charge transfer process promoter. Both mechanisms were assessed for Zinc-Rich Epoxy (ZRE) coatings in the presence of Carbon Nanotubes (CNTs) and exposure to a bioelectrolyte in order to study the evolution process during microbial corrosion conditions. The purpose of this study is to characterize in a comprehensive experimental platform the electrochemical response of a dual-protection zinc epoxy coating with different ratios of additive carbon nanotubes to active zinc particles upon exposure to a sulfate reducing consortium. Carbon nanotubes addition was found to affect both the prevailing mechanism at the coating interfaces and the formation of a biofilm at the coating surface that influenced the relatively dominance of the barrier protection mechanism. These multifunctional coatings with active particles could help to balance the charge transfer efficiency in terms of the sacrificial of zinc and barrier mechanisms, which influence biofilm formation and have potential consequences for biocorrosion on carbon steel.

## 1. Introduction

Most coatings used for microbiologically induced corrosion (MIC) in industry are designed to provide an effective barrier to inhibit corrosion processes and/or provide a biocidal effect. These coatings are synthesized using organic, inorganic, and hybrid approaches. Organic coatings have been demonstrated to provide an effective physical barrier in a variety of aggressive conditions (Abdolahi et al., 2014, Deflorian et al., 2005, Fedel et al., 2019). However, when exposed to anoxic conditions such as those prevailing in seawater or oil and gas pipelines, some of these coatings

42 degrade faster upon exposure to either a bacterial consortium or a specific strain of microbial attack  
43 (Enning and Garrelfs, 2014).

44 Unfortunately, inorganic and hybrid protective coatings on steel have also been proven to degrade  
45 when exposed to MIC in such anoxic conditions (Abdolahi et al., 2014; Enning and Garrelfs, 2014;  
46 Ciubotariu et al., 2015). Environmentally friendly coatings are being developed to improve their  
47 physicochemical properties to resist microbiological attack, either in aerobic or anaerobic  
48 conditions, while avoiding toxicity to the environment from the inherently toxic formulations of  
49 some coatings.

50 Recent coating research has investigated nano-architected sacrificial coatings as a new technology  
51 with dual protection mechanisms. The first is galvanic or cathodic protection, which is achieved  
52 by integrating electrochemically active particles into the organic coating matrix. The second  
53 protection mechanism is the classical barrier effect offered by a polymeric matrix. The addition of  
54 nanostructures such as carbon nanotubes (CNTs) can enhance both properties by influencing the  
55 interconnectivity of active particles and filling the voids created during synthesis of the coating in  
56 the polymeric matrix, as noted by Cubides and Castaneda (Cubides and Castaneda, 2016).

57 Zn-rich epoxy primers have shown excellent results and have been used by the industry since the  
58 60's and 70's (Weinell and Rasmussen, 2007). The mechanisms of corrosion protection in the Zn-  
59 rich epoxy primers include a galvanic effect due to metallic zinc dissolution, as well as a barrier  
60 effect resulting not only from the epoxy resin but also via the formation of Zn and Fe products  
61 (Deflorian et al., 2005, Weinell and Rasmussen, 2007). However, a balance must be considered in  
62 the formulation in order to assure cathodic protection for an extended time. A load of 90 wt.% of  
63 Zn particles may be beneficial for the charge transfer process (Park and Shon, 2015). However,  
64 that amount can reduce substrate adhesion and cause problems with the spraying application  
65 related to the high viscosity and poor dispersion of zinc particles (Park and Shon, 2015). Hence,  
66 research has sought to decrease the percentage of Zn load while retaining the connection among  
67 the particles and maintaining or increasing mechanical coating properties (Weinell and  
68 Rasmussen, 2007; Park and Shon, 2015; Jeon et al., 2013).

69 Weinell and Rasmussen (Weinell and Rasmussen, 2007) noted that different pigments, such as  
70 thixotropic agents, can be added to the epoxy matrix of coatings to prevent zinc precipitation. The  
71 authors incorporated colored pigments to differentiate between steel substrate and the greyish Zn  
72 primer, adding oil-absorbing pigments to decrease the Zn load while maintaining the same level  
73 of cathodic protection. Park and Shon suggested the addition of multiwalled carbon nanotubes  
74 (MWCNTs) to a maximum load of 0.6 wt.%, which resulted in improved conductivity, adhesion  
75 strength, and corrosion protectiveness as the MWCNTs increased from 0 to 0.25 wt.% (Park and  
76 Shon, 2015). Similarly, the addition of MWCNTs in an epoxy coating provided greater adhesion  
77 strength, transport behavior, and hydrophobicity as the MWCNT concentration increased from 0  
78 to 0.5 wt.% (Jeon et al., 2013).

79 The microbiological environment and underlying mechanisms have not been extensively explored  
80 in coating studies of Zn-rich epoxy primers. A few studies have evaluated Zn-rich epoxy primers  
81 in media containing sulfate reducing bacteria (Wang et al., 2012; Liu et al., 2007), but to the best  
82 of our knowledge no studies have investigated Zn-rich primers with MWCNTs added to their  
83 matrix in an environment including a sulfate reducing consortium.

84 This work aims to determine the electrochemical behavior of a Zn-rich primer with MWCNTs  
85 additions in an electrolyte containing an SRM consortium. Electrochemical techniques were used  
86 to elucidate the interfacial mechanisms. We used electrochemical impedance spectroscopy as a

87 primer technique to characterize the mechanisms presented at different interfaces formed in the  
 88 system, and the results were analyzed using electrical analog element coupled with high-resolution  
 89 surface techniques. Different CNTs compositions were used to support the influence of the  
 90 mechanism's dominance based on the corrosion control method.

91  
 92

## 93 2. Materials and Methods

### 94 2.1 Microbial culture

95 The consortium of sulfate reducing bacteria (sulfate reducing microorganisms) used in this study  
 96 was collected with an in-line inspection tool used for internal inspection in pipelines (the so-called  
 97 smart 'PIGS'). The sample consortium was inoculated in ATCC1250 modified Baar's medium for  
 98 Sulfate Reducers with NaCl (2.5 wt.%) [ATTC®]. The pH value was adjusted to 7.2 under de-  
 99 aeration by applying nitrogen to the electrolyte. The medium was autoclaved at 120°C for 15 min.  
 100 The SRM consortium was incubated at 37°C.

### 101 2.2 Multifunctional Coatings.

102 The Zn-rich epoxy primers and multiwalled carbon nanotubes were supplied by Tesla  
 103 NanoCoatings company. The epoxy resin (Tesla P1150ASAS) was mixed with CNTs at 1 and 2  
 104 wt.%. After the CNTs were completely dispersed in the epoxy resin through mechanical stirring  
 105 according to a previously method (Cubides and Castaneda, 2016), Zn particles at 70 wt.% were  
 106 slowly added while stirring the solution, and a hardener (Tesla P1150BSAS) was then poured in  
 107 to a final weight ratio of 2:1 (epoxy resin-hardener). The 70 wt. % was used based on the previous  
 108 work (Cubides and Castaneda, 2016) where is was demonstrated the Zn content was the most  
 109 balanced for cathodic protection or sacrificial conditions. In addition, Zn-rich epoxy primer  
 110 without CNTs was also used in this study. The coatings were air-sprayed onto UNS1008 steel  
 111 plates. This procedure was performed previously (Cubides and Castaneda, 2016). Table 1 shows  
 112 the different sample characteristics.

113 Table 1. Specifications of the different coating systems.

114 Table 1. Specifications of the different coating systems.

Coating	Zinc (wt.%)	(CNTs) (~wt.%)
ZnR	70	0
Zn-1CNT	70	1.0
Zn-2CNT	70	2.0

115

### 116 2.3 Electrochemical characterization.

117 A three-electrode electrochemical cell was used for the experimental characterization. The  
 118 electrochemical cells were autoclaved. The working electrode was the multifunctional coating  
 119 sample. The counter electrode was a platinum mesh, and the reference electrode was a saturated  
 120 calomel electrode (SCE). The working electrodes and the reference and auxiliary electrode were  
 121 sterilized with 70% ethanol and acetone and set under UV light and laminar flow. They were  
 122 placed on a 25 mL electrochemical cell containing culture medium under N<sub>2</sub> gas injection before  
 123 each experiment. It was conducted at 25°C. OCP was performed on prior EIS measurements during

128 a period of 10 minutes. EIS was performed in a frequency range of 100 KHz to 10 mHz with a  
129  $\pm 10$  mV peak-to-peak amplitude vs. the open circuit potential (OCP). All the tests were carried out  
130 in a potentiation/galvanostat (VSP-300; Bio-Logic Science Instruments), using the software EC-  
131 Lab® V.10.32. All electrochemical experiments were performed in duplicate to ensure  
132 reproducibility of the electrochemical behavior.

133

134

### 135 2.4 SEM sample preparation.

136 Once the electrochemical test was completed, the samples were rinsed with PBS 1X (8.0 g of NaCl,  
137 0.2 g of KCl, 1.4 g of  $\text{Na}_2\text{HPO}_4 \cdot 2\text{H}_2\text{O}$ , and 0.2 g of  $\text{KH}_2\text{PO}_4$  per liter, pH= 7.2). Subsequently, the  
138 samples were fixed with glutaraldehyde 2.5% w/v in PBS for 2 h, with washing every 30 min. All  
139 fixation was conducted at room temperature. After fixation, the cells were washed twice in PBS  
140 and then re-suspended in sterilized ultrapure water to avoid salt crystallization during the drying  
141 process. The samples were dried for 24 h in a LABCONO Freezone 6 lyophilizer. Finally, the  
142 samples were sputtered with silver particles and observed under a JSM-7000F/JOEL microscope  
143 through energy-dispersive spectroscopy (EDS).

144

## 145 3. Results and Discussion

### 146 3.1 Open circuit potential

147 The ZnR coating system shows the potential evolution influenced by different conditions and  
148 interfacial configurations such as the epoxy physical barrier, the galvanic phenomenon between  
149 zinc and steel, the physicochemical barrier of corrosion products, the concentration of Fe and Zn  
150 near the particle/coating or substrate/coating interfaces and inside the coating, amongst other  
151 factors, as described by Cubides (Cubides and Castaneda, 2016). The cathodic protection of steel  
152 has been established at  $\leq -0.90$  V vs. Cu/CuSO<sub>4</sub> (-0.826 vs. SCE) under anaerobic conditions  
153 (Schwerdtfeger, 1958; Guang et al., 2016; Liu and Cheng, 2017). This level is drawn as a dash line  
154 in Figure 1. At higher (more positive) potentials, barrier protection tends to be the dominant control  
155 mechanism, which may be associated with the epoxy-polymer and the corrosion products of Zn  
156 and/or Fe. The OCP monitoring of the AISI/SAE 1008 steel substrate and the multifunctional  
157 coatings under biotic conditions is shown in Figure 1. The OCP for the bare steel is more positive  
158 (passive region or protective layer region based on thermodynamics) than the cathodic potential  
159 criteria because the galvanic effect results in a negative potential value, in which the steel faces  
160 immune thermodynamic conditions. The OCP for the bare steel 1008 was determined in a test  
161 where the sample was kept in the culture medium in bacterial consortium conditions, and the steel  
162 potential was found to be influenced by the biofilm and corrosion products formed at the surface  
163 of the substrate. Classic work by Castaneda (Castaneda and Benetton, 2008) characterized mild  
164 steel in seawater in the presence of SRB, which resulted in positive potentials due to the  
165 combination of corrosion products and biofilm. Figure 1 shows the initiation and growth stages  
166 for the biofilm formation. At this respect, Castaneda marked 14 days for the initiation to biofilm  
167 growth transition, similar to this condition, where the OCP increases the magnitude following two  
168 weeks of exposure.

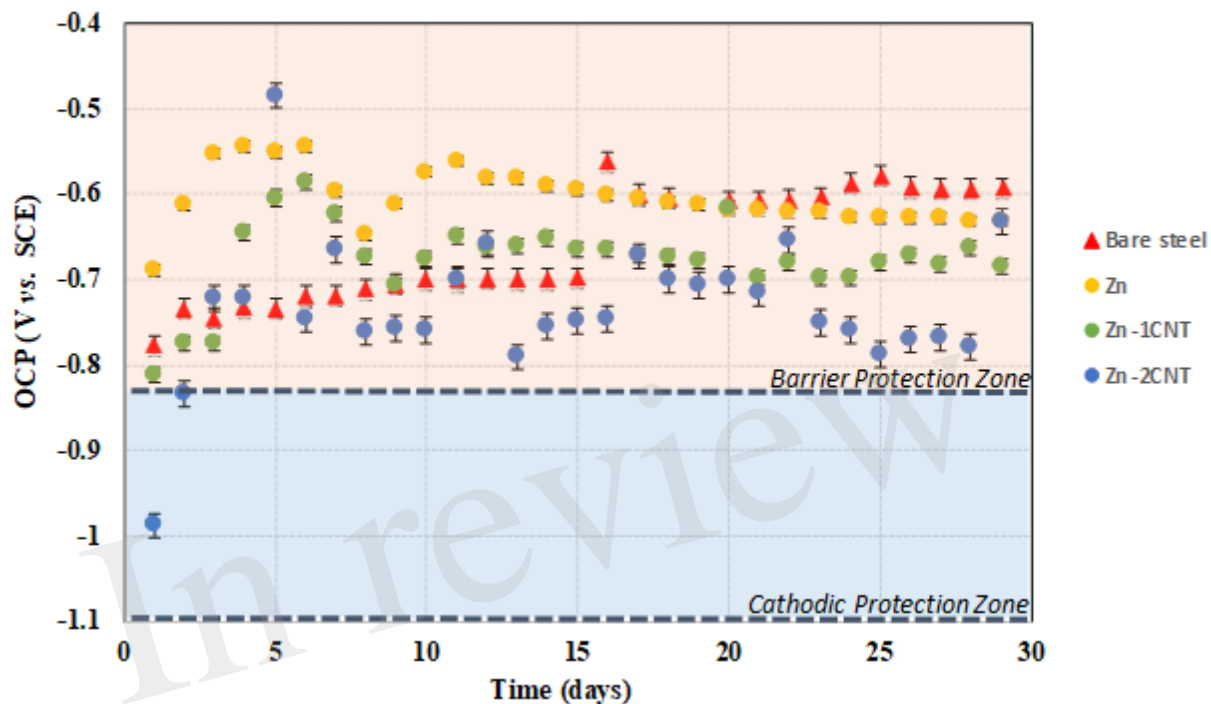
169 The Zn-rich primer (70 wt.% Zn) exposed to the bacteria consortium shows a potential oscillating  
170 within the barrier protection zone over the exposure time. This means that the Zn particles are

171 randomly distributed in the epoxy matrix with a connectivity between them that is insufficient to  
172 trigger the galvanic effect formation. There is a transient state during the first 10 days of exposure,  
173 and during this time, the potential values are in the barrier zone. This behavior is associated with  
174 water uptake in the coating and the formation of Zn products during the initial days of exposure.  
175 Finally, the potential is around the OCP of 1008 carbon steel in biotic conditions, but both  
176 experimental results are above the corrosion protection located in the barrier protection zone, and  
177 barrier zone dominance can result from the Zn-Fe corrosion products and/or biofilm formation to  
178 produce a blocking effect for the water uptake process.

179 At the early stage, the Zn-1CNT potential is located close to the cathodic protection zone for the  
180 first day. Following the negative potentials, a transient stage occurs during the next 10 days within  
181 the barrier protection area. The initial conditions could be the response of the bioelectrolyte wetting  
182 over the Zn particles and due to the interconnectivity among Zn particles and steel arising from  
183 the influence of MWCNTs or the cathodic protection effect; the potential between 4 and 10 days  
184 may be the result of Zn and/or Fe corrosion products acting as a barrier or passive particle state,  
185 which switches the system to prevail in more positive potentials. These latter compounds fill the  
186 porous surfaces within the coating structure, and the potential subsequently increases at day 2. The  
187 interaction between consortium/coating subsequently changes the quantity and morphology of the  
188 products, and the potential decreases at day 10. Eventually, the potentials reach approximately -  
189 0.680V vs. SCE in the barrier zone, 100 mV more negative than the ZnR sample. Subsequently,  
190 the potential remains stable at close to -0.680V vs. SCE. This latter effect could be due to the  
191 influence of the biofilm at the surface, in which the zinc ions inhibit the formation of the biofilm  
192 layer at initial conditions (Babich and Stotzky, 1978, Bong et al., 2010, Billanger et al., 2015,  
193 Tong et al., 2015), but the ions are depleted and the biofilm starts to grow over time to become  
194 more homogeneous and distributed compared with the 2CNT, and the magnitude of the potential  
195 becomes more negative than the ZnR sample to produce a less dominant barrier effect with the  
196 addition of 1CNT.

197 OCP for the Zn-2CNT sample are more negative than the threshold for the cathodic protection  
198 magnitude during the first 2 days. This behavior is associated with a greater MWCNTs  
199 concentration, resulting in better interconnection between the Zn/Zn electrical connection particles  
200 due to the CNT/Zn/CNT interconnectivity. This latter finding is confirmed in the cross-section  
201 SEM images. These potentials are more negative than the Zn-1CNT results. A transient potential  
202 state exists between days 3 and 10 of exposure. After 10 days, there are two transient states during  
203 the barrier protection zone and close to the cathodic protection threshold, one between 10 and 15  
204 days and the other between 16 and 24 days. Finally, the potential keeps fluctuating in the barrier  
205 protection zone and reaches lower values than the OCP of carbon steel in biotic conditions. The  
206 potentials reveal the dominance of cathodic protection for this sample in different stages. Particle  
207 activation was promoted by the distribution of CNTs within the coating, and the products formed  
208 in the coating are not sufficiently compact to stop bioelectrolyte uptake within the coating, with  
209 the unstable biofilm leading to lower potential magnitudes. This may result from greater  
210 electrochemical activity among particle/coating interface. This latter result is evidence of a certain  
211 grade of galvanic effect, i.e., the system is at a lower potential than the value found for steel without  
212 coating due to reaction with the Zn particles. The presence of two increments may be due to the  
213 creation of products that fill the pores in the coating, with the decrease resulting from the particle  
214 layer and an interaction forming with an incipient heterogeneous biofilm. That is, zinc ion

215 formation inhibits biofilm growth and leads to various areas of biofilm depletion, thus affecting  
 216 the morphology of these compounds over time and altering the distribution of the biofilm at the  
 217 surface of the coating.



218  
 219 **Fig. 1. OCP for bare steel and the three different multifunctional coatings under bioelectrolyte**  
 220 **conditions**

### 221 3.2 Qualitative analysis of impedance

222 Figure 2 shows the complex and phase angle diagrams for Bare steel and Zinc Rich Epoxy  
 223 multifunctional coatings in SRM consortium environment.

224 The Nyquist representation for the AISI 1008 bare steel sample exposed to the biotic electrolyte is  
 225 shown in Figure 2(a). The results show a loop with a large diameter characteristic of a capacitance  
 226 and charge transfer process. The phase angle representation is illustrated in Figure 2(b). The  
 227 medium frequency response is associated with capacitance (double layer) at the surface, whereas  
 228 the response at low frequency is associated with the electrochemical reactions at the  
 229 steel/electrolyte interface. On day 5, this system represents biofilm formation, and the corrosion  
 230 products form an inorganic and organic mixing layer. At low frequencies, the magnitude of the  
 231 semicircle's diameter is associated with the substrate/mixing layer/electrolyte interface. The  
 232 magnitude for the biotic conditions results in a loop intercepting the locus point on the order of  
 233 12,000  $\Omega \text{ cm}^2$ , whereas at 10 days, an increase in the loop diameter occurs, which may be  
 234 associated with the accumulation of a mixing layer formed at the surface. At the surface, the  
 235 number of active sites decreases, and the  $R_{ct}$  increases, as previously described by Castaneda  
 236 (Castaneda and Dominguez, 2008), with mild steel exposed to an SRM electrolyte during the first  
 237 2 weeks. At day 15, the impedance magnitudes begin to decrease, reflecting an activation



238 mechanism, and an increase in the number of active sites occurs at the metallic substrate/mixing  
239 layer interface. On day 20, the impedance lowers the magnitude for this sample, an effect  
240 associated with the active sites, owing to the charge transfer process. After 25 days, the  
241 contribution of two potential interfaces is revealed by two maximum points in the phase angle  
242 representation. At days 25, and 29, the active sites remain constant, owing to the maintenance of  
243 the impedance at low magnitudes and the formation of two separate contributions at the interface  
244 layers, owing to the stability and physical presence of a mixing layer on the surface, as a result of  
245 precipitation of corrosion products and presumed biofilm formation. This finding corroborates the  
246 OCP biofilm transition from initiation to growth stage. The EC representation for this system can  
247 be described by Figure 3a and 3b; the first days include an activation capacitance RC analog, and  
248 after 25 days, two time constants are represented by two constant phase elements.

### 249 *3.2.1 Zinc Rich Epoxy*

250 The EIS results for the ZnR sample are shown in Figure 2(c) and 2(d). Two loops are observed:  
251 one at medium-high frequency and another at low frequency in the complex representation. In the  
252 phase angle representation, two time constants are observed, representing the interfaces due to the  
253 presence of a mixed layer (biofilm, epoxy coating) and the zinc particle/coating interface. Figure  
254 3b represents the equivalent circuit used for the ZnR epoxy/steel interface in the early stage. Part  
255 of this circuit has been proposed by Cubides to represent the ZnR on a metallic substrate system  
256 when the zinc particles are active after being exposed to an electrolyte, where  $R_s$  is the electrolyte  
257 resistance,  $R_p$  is the porous layer resistance formed by the coating,  $CPE_1$  is the constant element  
258 for medium frequencies,  $R_{ct}$  is the charge transfer resistance due to the active particle/coating  
259 interface,  $CPE_2$  is the constant phase element associated with the double layer capacitance, and  $n$   
260 is the roughness factor. (Cubides and Castaneda, 2016). In general, all the impedances are higher  
261 than those of the bare steel samples, as can be seen in Table 2. This is due to conductivity of the  
262 Zn-rich epoxy influenced by the polymer coating matrix. In addition, the impedance signal is  
263 influenced by several factors such as electrolyte uptake within the coating, the galvanic effect of  
264 the Zn particles, the relation between Fe/Zn areas exposed to electrolyte, product formation, and  
265 biofilm formation (Abreu et al., 1999; Galicia et al., 2017). The  $R_{ct}$  impedances in this case are  
266 within an order of magnitude at around 50,000–100,000  $\Omega\text{-cm}^2$  as illustrated in Table 2. This is in  
267 concordance with the OCP results in which the behavior of the systems is maintained at a specific  
268 potential zone. The semicircle acquired at the higher-medium frequency is associated with  
269 presumable coating-biofilm mixed layer, and the semicircle recorded at low frequency is the  
270 response of Zn/Epoxy interfacial reactions. The equivalent circuits describing the early stage of  
271 the system are illustrated in Figure 3b. The EC shows two time constant phase elements in parallel  
272 with two resistances representing early and continued evolution for 20 days. The time constants  
273 associated with the medium and low frequencies are consistent with the evolution of each element  
274 in the system. During the initial days, the electrolyte uptakes the coating and wetting of Zn  
275 particles, even though the galvanic effect prevailing at the particle/coating interface the overall  
276 OCP shows positive magnitudes away from the cathodic protection potential for anaerobic  
277 conditions, this latter can be attributed to the poor particles interconnection within the epoxy,  
278 resulting in a small area for the electrochemical reaction. The zinc particles react to produce ionic  
279 species and corrosion products; the zinc ionic species preserve the surface of the coating with no  
280 biofilm formation, likely due to a cytotoxic mechanism against microorganisms (Babich and  
281 Stotzky, 1978, Billanger et.al., 2015, Tong et.al., 2015). Two time constants are maintained for the

282 phase angle representation while the  $R_p$  and  $R_{ct}$  impedance in the complex representation increases  
283 up to 20 days. The wetting of the zinc particles following the charge transfer reactions no longer  
284 predominates, owing to the formation of corrosion products such as ZnO and  $Zn(OH)_2$  at the zinc  
285 particle/coating interface, as reported previously (Cubides et al., 2016). The production of  
286 extracellular polymeric substances (EPSs) apparently begins to influence the high impedance  
287 values revealed at high-medium frequencies. Subsequently, a mature biofilm forms a  
288 heterogeneous layer as illustrated in Figure 4(a) obtained by scanning electronic microscopy,  
289 SEM. After 20 days, the complex signature reaches a higher impedance magnitude, resulting in  
290 the capacitance EIS signature representation. This latter result is consistent with the phase angle  
291 representation with the formation of only one time constant at medium-low frequencies. The final  
292 layer is a mixture of EPS/biofilm, corrosion products and precipitates, which allows the capture of  
293 the influence of this layer in the frequency interval range. The phase angle identifies one time  
294 constant in the system with a magnitude of 60 degrees, closer to the ideal capacitor effect of 90  
295 degrees. This latter is attributed to a semi compact (heterogeneous) layer formed by mixture of  
296 organic epoxy, organic EPS/biofilm and corrosion products. The sample was evaluated at 29 days  
297 of bioelectrolyte exposure conditions. The Zn-rich epoxy illustrated in Figure 4(a) shows that the  
298 morphology is modified after exposure and demonstrates the underlying mechanisms; the sample  
299 shows the presence of a heterogeneous Extracellular Polymeric substances on the electrode as a  
300 biofilm. The balance between the Zn presence and the biofilm formation produce a biolayer of  
301 12.5  $\mu\text{m}$  in thickness.

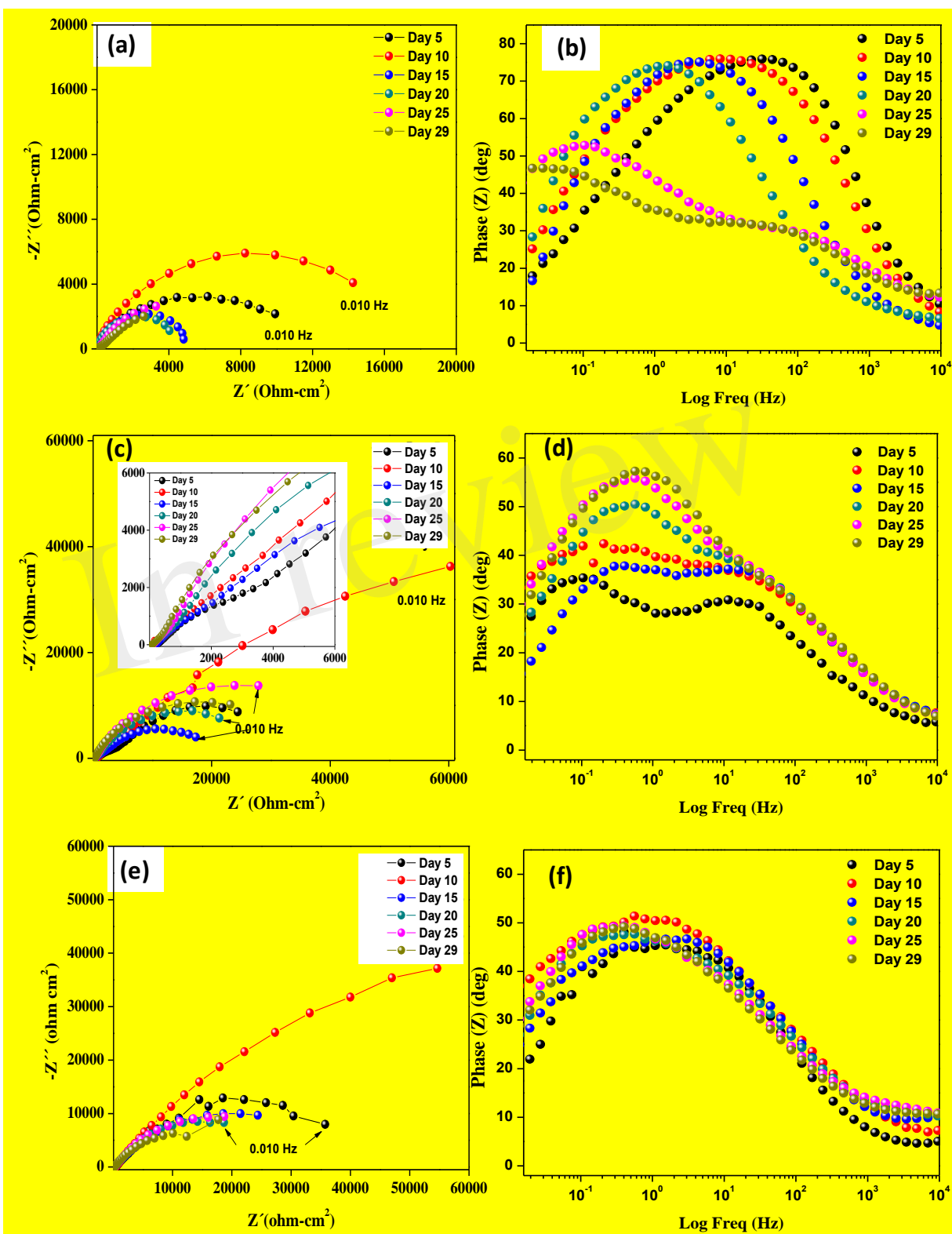
302

### 303 **3.2.2 Zinc Rich Epoxy with 1CNT**

304 The Nyquist diagram of the Zn-1CNT is displayed in Figure 2(e) for the complex representation  
305 and 2(f) for the phase angle. There is one loop with a finite locus point in the real axis, owing to  
306 the capacitance behavior and charge transfer reaction step control process at the zinc/coating  
307 interface. At day 5, the  $R_{ct}$  impedance magnitudes in the EIS signature are similar in magnitude to  
308 those of the ZnR epoxy samples. The electrical interconnection between Zn particles is increased  
309 with the addition of CNTs, which in turn favors the formation of products within the coating  
310 through favoring the charge transfer reaction at the Zn/coating interface, and the level of protection  
311 subsequently improves, as corroborated by the OCP in early stages. The presence of the CNTs  
312 promoted zinc particle area/substrate or particle/particle interactions; initially, charge transfer  
313 process kinetics are favored due to the area available for galvanic reactions. The initial presence  
314 and distribution of extracellular polymeric substances was influence by Zn leaching and  
315 precipitation within the coating as well as precipitation at the surface of the corrosion products.  
316 EPS formation and subsequent biofilm stability was influenced by the amount of reacted zinc at  
317 the particle/coating interface. Following system evolution, changes in the corrosion products and  
318 growth of the biofilm shifted the charge transfer magnitude. Competition between formation of  
319 the biofilm on the surface and the corrosion products within the coating is balanced by the  
320 formation of zinc ions and influenced by the amount of CNTs. The SEM image in Figure 4(b)  
321 shows a smaller biofilm thickness on the coating surface after 29 days of exposure when the  
322 concentration of CNTs stayed at 1CNT. The impedance gain could mark a transition moment of  
323 the system, which does not follow the EIS application principle of stability (Bosch et al., 2001)  
324 because the OCP for the sample decreased significantly at 10 days. However, the subsequent

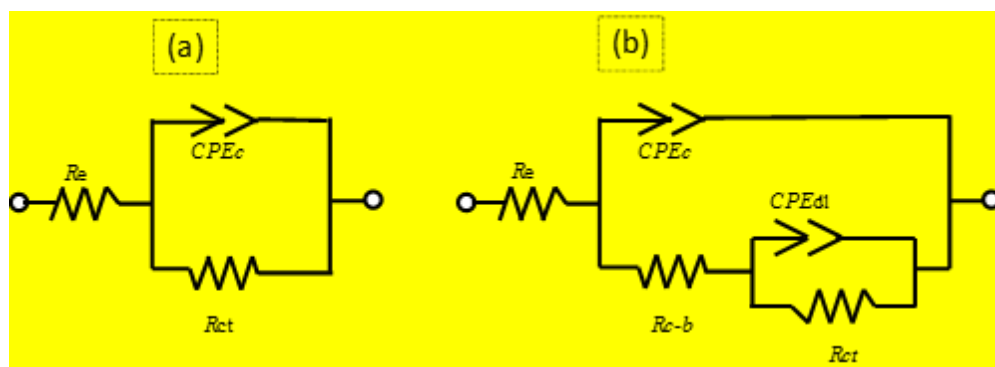
325 exposure times at 15, 20, and 25 days exhibit an increase in charge transfer resistance, or  $R_{ct}$ , which  
326 agrees with the OCP results. The 1CNT concentration influences the EPS, biofilm formation and  
327 mix layer, by dissolution or inhibition mediated by the Zn ions and the kinetics of the corrosion  
328 products formed at the Zn particle interface. This latter result is due to the decrease in Zn ionic  
329 formation caused by surface de-activation of particles and their depletion resulting from their usage  
330 in the formation of corrosion products, with the decrease also due to biofilm inhibition (Babich  
331 and Stotzky, 1978, Bong et al., 2010). The presence of one time constant in the phase angle  
332 representation for Zn-1CNT reflects the influence of capacitive behavior resulting from a mixture  
333 of the organic coating, inorganic corrosion products and biofilm. This indicates that a mix layer  
334 was formed on top of the coating, as evidenced by the impedance signature of Figure 2(f) and SEM  
335 image of Figure 4(b). The morphology of the biofilm is very different from that of with zinc-rich  
336 sample. The Zn products were obtained with a higher density, the corrosion products expanded the  
337 ZnR coating in some locations, and the biofilm was no continuous compared with ZnR. For Zn-  
338 1CNT, the phase angle shows one-time constant appearance at early stage. The early stage at OCP  
339 correlates interconnectivity of the CNTs, with active zinc particles reacting faster compared to  
340 without the CNTs

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342 **Fig. 2.** Diagrams of Nyquist and phase angle in the SRM consortium for (a)-(b) 1008 bare steel,  
 343 (c)-(d) for ZnR coating, and (e)-(f) for Zn-1CNT coating.



344  
345 **Fig. 3.** Equivalent circuits proposed for the interface evolution on the basis of the interfacial  
346 components

347  
348 **Table 2**

349 **Fitting parameters from an equivalent circuit simulation for AISI 1008 bare steel**

Circuit element → Time (day) ↓	$R_e$ ( $\Omega\text{-cm}^2$ )	$CPE_1$ ( $F\text{ cm}^{-2}$ )	$\alpha$	$R_c-b$ ( $\Omega\text{-cm}^2$ )	$CPE_2$ ( $F\text{ cm}^{-2}$ )	$R_{ct}$ ( $\Omega\text{-cm}^2$ )
5	4.7	1.5E-04	.8	-	-	11987
10	5.0	1.7E-04	.8	-	-	15090
15	5.7	4.2E-04	.8	-	-	5254
20	7.1	8.6E-04	.8	-	-	5137
25	9	7.1E-04	.5	315	4.1E-04	16554
29	22	1.7E-05	.5	977	8.7E-04	12352

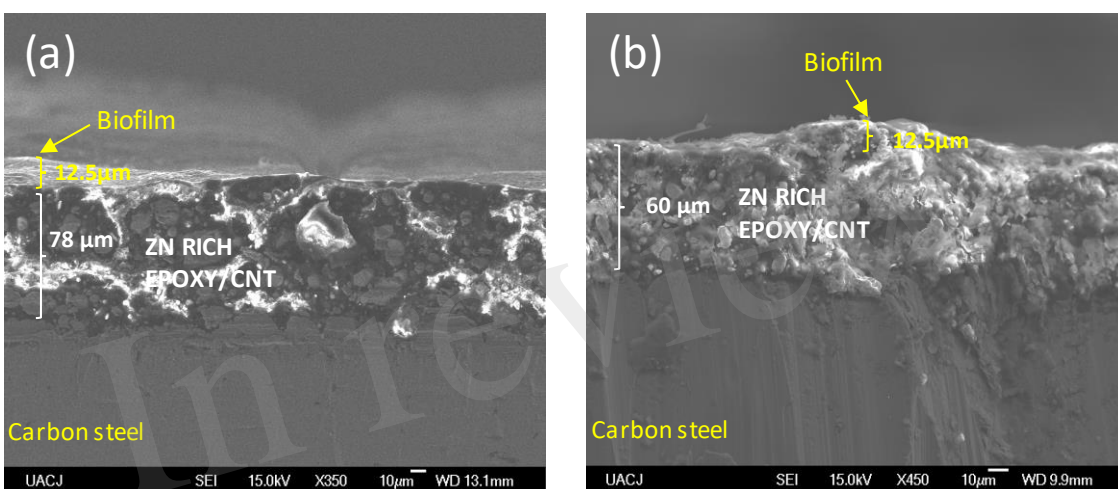
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351 **Table 3**

352 **Fitting parameters from an equivalent circuit simulation for multifunctional coatings**

Circuit element → Time (day) ↓	$R_e$ ( $\Omega\text{-cm}^2$ )	$CPE_1$ ( $F\text{ cm}^{-2}$ )	$\alpha$	$R_c-b$ ( $\Omega\text{-cm}^2$ )	$CPE_2$ ( $F\text{ cm}^{-2}$ )	$R_{ct}$ ( $\Omega\text{-cm}^2$ )
<b>ZnR</b>						
5	502	8.5E-07	.5	21204	5.7E-07	39143
10	400	4.6E-07	.5	175716	6.8E-07	53761
15	205	9.8E-07	.5	23631	1.3E-06	1203
20	171	1.2E-04	.6	29509	5.8E-07	5654
25	138	1.1E-04	.7	-	-	29245
29	85	2.1E-04	.7	-	-	26936
<b>Zn-1CNT</b>						
5	400	8.9E-07	.6	-	-	39001
10	426	5.4 E-07	.6	-	-	50038
15	183	1.0E-02	.6	-	-	37817
20	139	1.4 E-02	.6	-	-	33855
25	132	1.6 E-02	.6	-	-	39595
29	109	2.2 E-02	.6	-	-	39516
<b>Zn-2CNT</b>						

5	290	5.0E-07	.6	-	-	77908
10	157	1.0E-05	.6	-	-	35247
15	125	6.7E-05	.6	-	-	43741
20	123	7.2E-05	.6	-	-	42736
25	138	9.2E-05	.6	-	-	43580
29	49	3.1E-04	.6	-	-	13532

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**Fig. 4.** Cross-section SEM images of the coatings immersed in an electrolyte with the SRM consortium. (a) Zn rich-primer, (b) Zn-rich primer with 1 wt.% CNTs

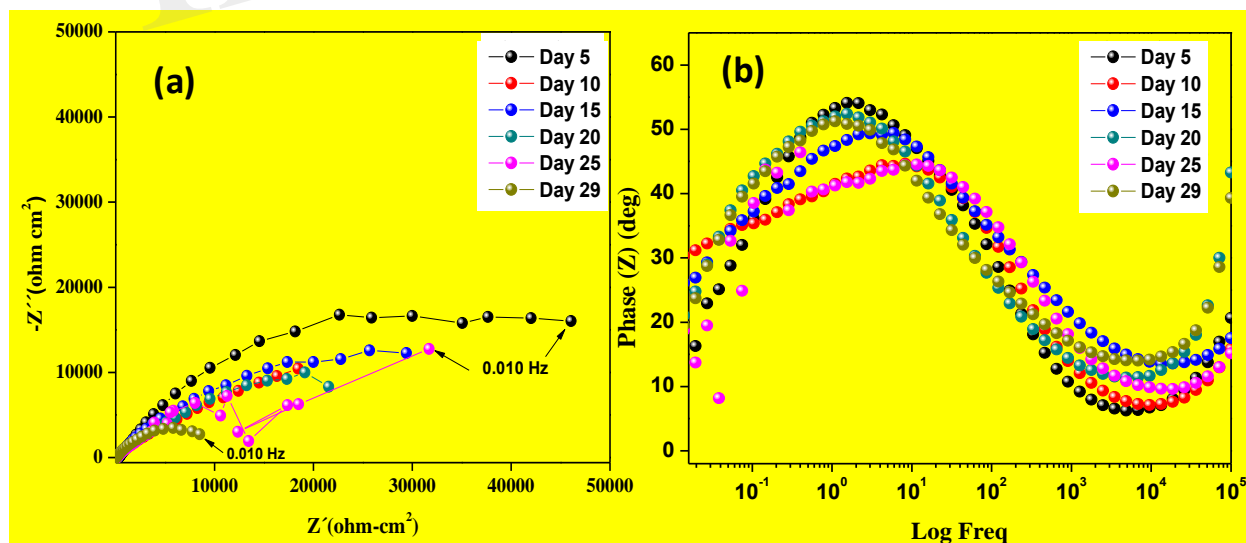
### 3.2.3 Zinc Rich Epoxy with 2 CNT

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The impedance signature of the Zn-2CNT sample is exhibited in Figure 5(a) and 5(b). There is one loop for the complex representation and one time constant for the phase angle signature. The electrical connection among the Zn particles is evident in the OCP results, and this is associated with a Zn area that is much greater than the Fe iron exposed to the electrolyte, which is due to the increased CNTs content. The EIS signature corroborates the formation/initiation of EPS and the biofilm as well as the charge transfer dominance due to Zn particle activation, resulting in corrosion products within the coating. The formation of corrosion products at the particle/coating interface should be favored due to the higher electronic interconnectivity. However, the biofilm does not form homogeneously due to the presence of Zn products formed from bulk zinc ion generation from the coating and their transport to the coating surface. **The substantial CNT content surpasses the ionic Zn content that inhibits biofilm formation. After 10 days, the impedance magnitude decreases, owing to the activation of Zn particles. At day 29, the system evolves to the lowest charge transfer resistance,  $R_{ct}$  magnitude. The CNT increases the Zn particle kinetics and avoids continuous formation of a mixed layer that does not appear at this concentration.**

377 The impedance analysis gave insight into the competition among anodic dissolution of zinc  
 378 particles, EPS/biofilm formation, and the formation of zinc-rich corrosion products. Phase angle  
 379 representation shows one time constant. The signature is characteristic of capacitive process and  
 380 controlled by charge transfer resistance. The time constant at medium frequencies may represent  
 381 the influence of a capacitance of a unified (mixed) layer forming at the surface, and the low  
 382 frequency characterizes the particle/coating interface. With time, anodic dissolution of Zn and the  
 383 formation of Zn corrosion products become less prevalent, and thus do not provide sufficient  
 384 protection to the metal substrate. From the Nyquist plot, the impedance of the ZnR coating  
 385 increased with time. Great influence in resistance is attributed to the EPS/biofilm formation noted  
 386 above in combination with inorganic semiconductor ZnO and Zn(OH)<sub>2</sub> corrosion products  
 387 following Zn dissolution, which provides added barrier. EIS analysis agrees with the OCP  
 388 measurement findings in that the addition of CNTs to the polymeric matrix structure improves the  
 389 electrical connectivity between zinc particles and the metallic steel substrate through electron  
 390 transport. In early stages, both the Zn-1CNT and Zn-2CNT coated samples showed potential below  
 391 the CP threshold potential. SEM images after 28 days of immersion in Figure 7, suggest that the  
 392 biofilm forms at the early days of immersion and subsequently grows/inhibits based on the Zn  
 393 content generated by the more efficient galvanic system. The limited presence of an  
 394 exopolysaccharide matrix, along with the limited population of bacteria and other organisms,  
 395 accounts for the possibility that biofilm limited formation at the surface occurred, in part due to  
 396 the presence of carbon nanotubes for Zn-1CNT and Zn-2CNT.  
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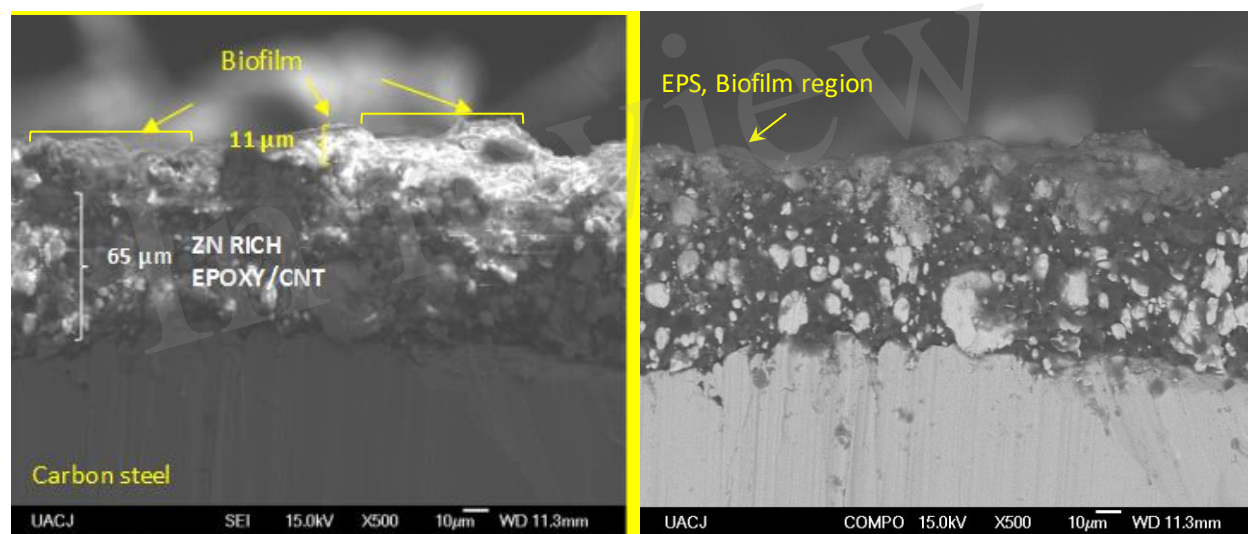
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399 **Fig. 5.** Diagram of Zn-2CNT coating in the SRM consortium: Nyquist (a) and phase angle (b)  
 400 representations.  
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404 The SEM image of a Zn-2CNT sample in Figure 6 shows several regions with biolayer removal  
 405 and some residual Zn particles in the epoxy. This Zn-2CNT sample has the thinnest randomly  
 406 distributed biofilm formed at the top of the coating surface. This latter result, could be attributed  
 407 to the dissolution of zinc particles, which form ZnCl<sub>2</sub> or ZnO that presumably inhibit initial biofilm

408 formation by poisoning certain cellular elements present in microorganisms (Tong et al.). Many  
 409 investigations have demonstrated that zinc cations, zinc oxides and zinc chlorides are cytotoxic by  
 410 disturbing gene regulation processes associated with the production of extracellular polymeric  
 411 substances (EPSs) (Babich and Stotzky, 1978, Billanger et.al., 2015, Tong et.al., 2015). The above  
 412 factors prevent construction of the matrix component of the biofilm. OCP and EIS results were  
 413 able to demonstrate initiation of the biofilm or mixed layer formation due to the transient state  
 414 revealed by both techniques over time. The shifts in OCP, magnitude and impedance elements  
 415 associated with the system interfaces accompanied trends including formation of the biofilm is a  
 416 clear indicator of the influence by the CNT in terms of corrosion control mechanism. Zn ions  
 417 formed following CNT addition, which are then transported into the coating and inhibit biofilm  
 418 formation in locations with a higher density of Zn particles, the Zn and CNT content can be balance  
 419 to establish a critical magnitude or Zn/CNT ratio for the efficiency of the ZRE epoxy coatings.  
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422 **Fig. 6.** Cross-sectional SEM images of the coatings immersed in an electrolyte with the SRM  
 423 consortium. Zn-rich primer with 2 wt.% CNTs. Morphology of the image and a back scattered  
 424 electron image.  
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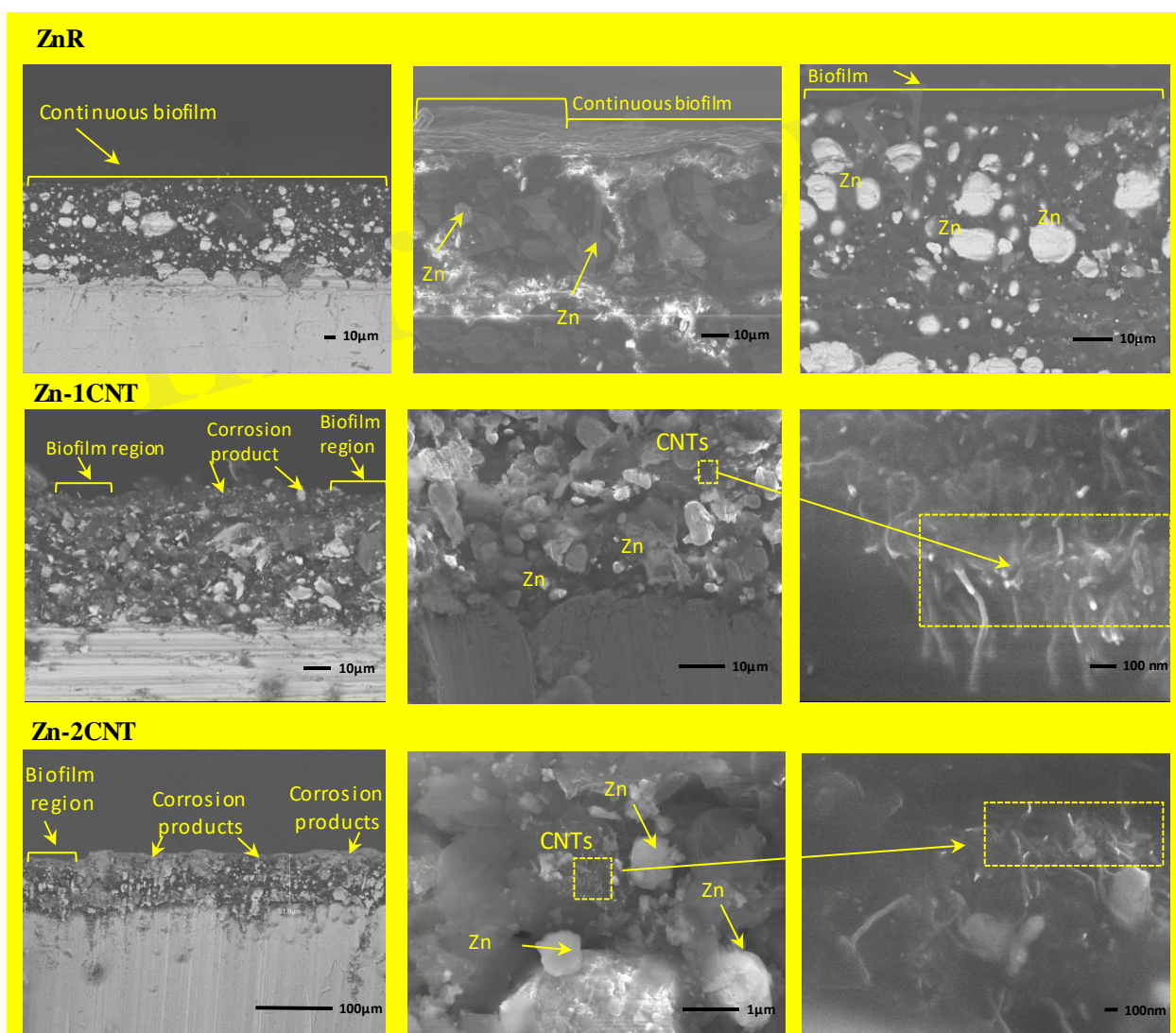
### 428 3.3 Surface evolution (top and cross section) characterization before and after 429 bioelectrolyte exposure

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 431 Figure 7 shows the cross-section SEM images obtained for the multifunctional coatings after 29  
 432 days of immersion in the SRM bioelectrolyte. These images corroborate the findings from the OCP  
 433 data and the impedance analysis. For Zn-1CNT and Zn-2CNT coatings, it was possible to detect  
 434 and demonstrate the presence and interconnectivity of Zn particles with carbon nanotubes at the  
 435 interface of carbon steel, the coating matrix itself and the EPS/corrosion product layer. **The biofilm  
 436 layer can be considered to provide greater extension for the ZnR coating because, as described  
 437 above, the CNT content leads to cytotoxicity toward the main bacterial and fungal constituents of**



438 the SRM consortium (Upadhyayula and Gadhamshetty, 2010). The increase in CNT content  
 439 promotes the formation of Zn ions, thus resulting in a cytotoxic environment. The images in Figure  
 440 7 reveal biofilm patch formation instead of a continuous layer at the electrode surface. Therefore,  
 441 the presence of biofilm is not favored when CNTs are present.  
 442

443 The presence of CNTs, as evident in Figure 7, was associated with an excellent influence on  
 444 conductivity at the inner section of the coating according to the impedance analysis. Lack of  
 445 uniform layer is ascribable to the dissolution of zinc cations, which are presumably cytotoxic to  
 446 the microorganisms. In turn, zinc ions could be also responsible for the formation of corrosion  
 447 products such as ZnO and ZnCl<sub>2</sub>, also the presence of these corrosion products also became evident  
 448 according to the EDS elemental analysis, this latter illustrated in Figure 8.



449 **Fig. 7.** Cross-section SEM images of the multifunctional coatings immersed in an electrolyte  
 450 solution with the SRM consortium: Zn rich-primer, Zn-rich primer with 1 wt.% CNTs and Zn-rich  
 451 primer with 2 wt.% CNTs.  
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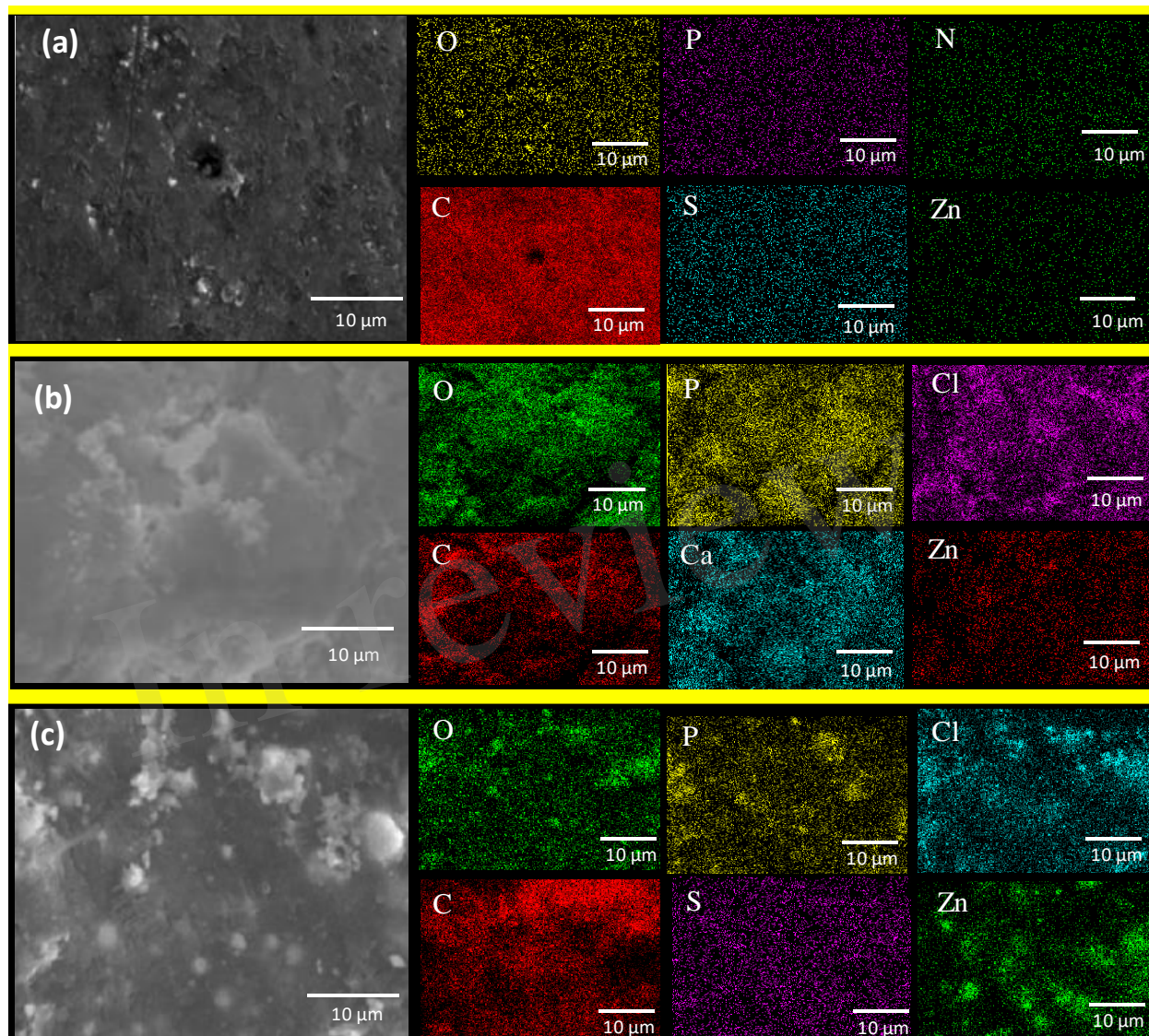
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455 Figure 8(a) to Figure 8(c) show top-view SEM images of the three multifunctional coatings after  
456 29 days of immersion in bioelectrolyte. For ZnR in Figure 8(a), a continuous layer of extracellular  
457 polymeric substances is observed covering the surface, which becomes less evident in the presence  
458 of CNT particles. Figure 8(b) illustrates the initial formation and lack of persistence of a layer of  
459 biofilm that shows some heterogeneous and residual over time. This finding is attributable to the  
460 inhibition of mature biofilm formation by the CNTs influence along with a poisoning mechanism  
461 by the cytotoxic effect of Zn soluble products (Babich and Stotzky, 1978, Bong et al.) At this  
462 respect, CNTs are considered to have adverse effects on biofilm growth at some levels according  
463 to the investigations of Upadhyayula and Gadhamshetty (Upadhyayula and Gadhamshetty, 2010).  
464 When a double content of CNTs is present, a greater porosity can be appreciated as shown in  
465 Figure 8(c), which is mainly attributed to the lack of continuous biofilm layer caused by an  
466 increased level of zinc corrosion products and the double content of carbon nanotubes that alter  
467 the development and formation of a mature biofilm.

468

469 Also, Figure 8(a)-8(c) show the EDS analysis demonstrating that the ZnR coating has a higher  
470 content of organic compounds, such as carbon, sulfur, nitrogen, and phosphorous (C, S, N and P)  
471 due to presence of a more mature biofilm, which supports the OCP data and impedance results.  
472 For the Zn-1CNT and Zn-2CNT coatings, a higher content of Zn and O is evident, and a lower  
473 level of organic compounds is found. Higher Zn levels indicate the formation of zinc corrosion  
474 products over the coating surface. In addition, the Zn-1CNT and Zn-2CNT coatings exhibit higher  
475 Zn and O content, thus further indicating that these coatings inhibit the formation of extracellular  
476 polymeric substances (Babich and Stotzky, 1978, Bong et al., 2010, Billanger et al., 2015, Tong  
477 et al., 2015), and therefore disturb biofilm growth to a greater extent due to the toxicity of the high  
478 levels of CNTs (Upadhyayula and Gadhamshetty, 2010).

479



481  
482 **Fig. 8.** Top views and EDS mapping analysis showing coatings samples after 29 days of exposure  
483 to the SRM consortium, (a) ZnR, (b) Zn-1CNT, and (c) Zn-2CNT. ZnR coating has a high content  
484 of organic compounds, such as carbon, sulfur, nitrogen and phosphorous (C, S, N and P) due to  
485 biofilm formation.

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#### 488 4 Conclusions

489

490 This investigation determined that for these multifunctional coatings, the anodic dissolution of  
491 zinc particles, the formation of an extra biolayer and the formation of zinc-rich corrosion products  
492 represent competing processes. The contribution of an extra layer formed on the coating surface  
493 can be attributed to the formation of EPSs and a biofilm by the SRM consortium. The CNTs  
494 content enhances the anodic reactions of the zinc particles in the coatings, promoting cathodic

495 protection and the formation of more corrosion products in the form of solid oxide/hydroxide  
496 compounds. However, doubling the CNT content results in more interaction with the zinc particles  
497 and impairment of biofilm growth. This represented a qualitative influence of CNTs concentration  
498 as evidenced by reduced levels of corrosion products. The ZnR coating exhibits galvanic  
499 protection, as evidenced by the formation of corrosion products and secretion of extracellular  
500 polymeric substances to produce a more homogeneous biolayer. The Zn-1CNT coating exhibits  
501 partial cytotoxicity towards microorganisms, thereby controlling biofilm initiation and growing  
502 processes. The Zn-2CNT ratio represents the saturated concentration of carbon nanotubes leading  
503 to less-optimal conditions for biofilm formation. Finally, we considered to be a CNTs content that  
504 could be used to balance biofilm formation and zinc anodic dissolution to influence  
505 microbiologically induced corrosion mechanisms.

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513

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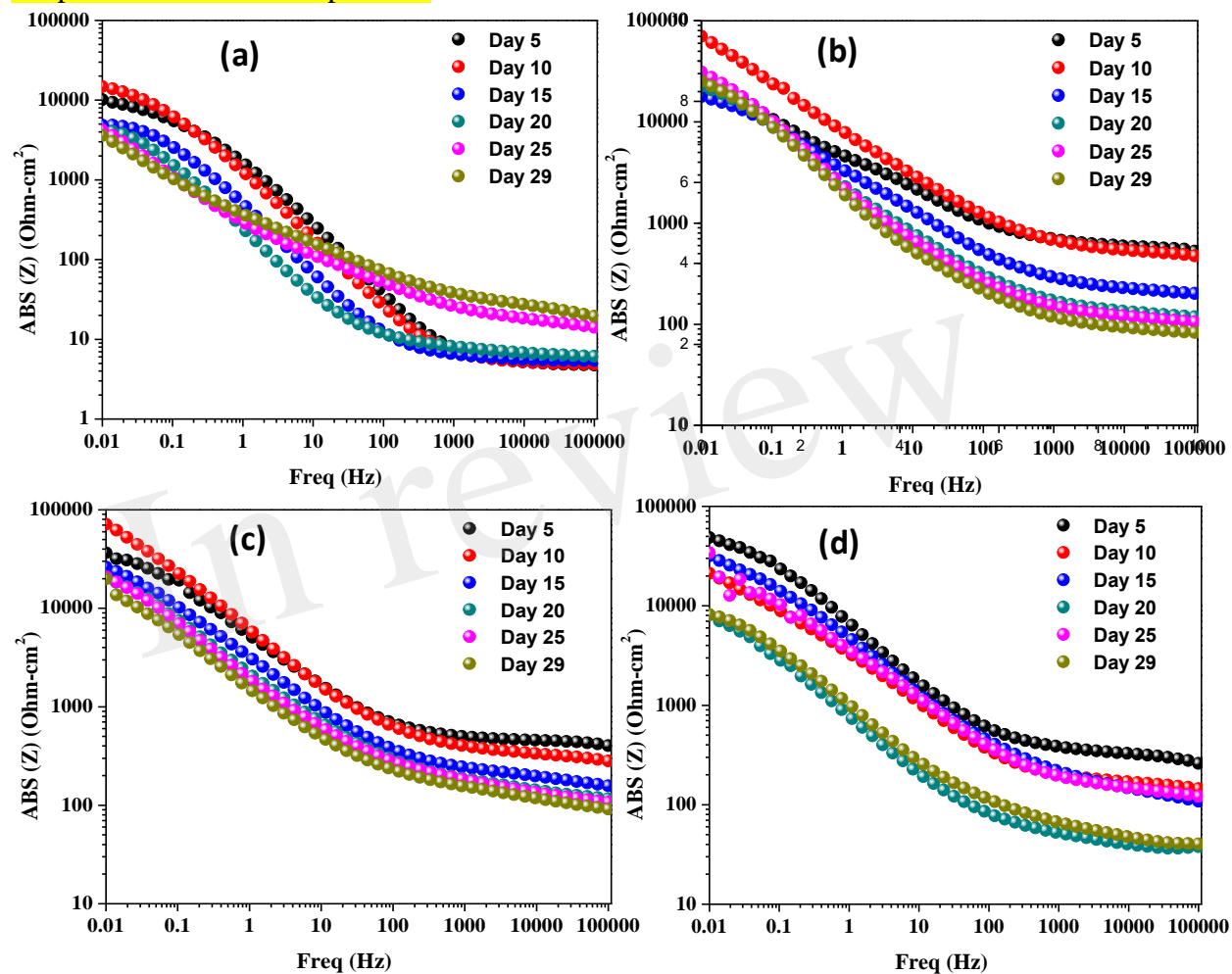
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Supplementary Material

Graphs for Module of Impedance



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Diagrams of Module of Impedance in SRM consortium for (a)1008 Bare steel , (b)ZnR coating, (c)Zn-1CNT coating, and (d) Zn-2CNT coating.

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